



# Absorption Measure Distribution in Active Galactic Nuclei

T. P. Adhikari  
Nicolaus Copernicus Astronomical  
Center, Warsaw, Poland  
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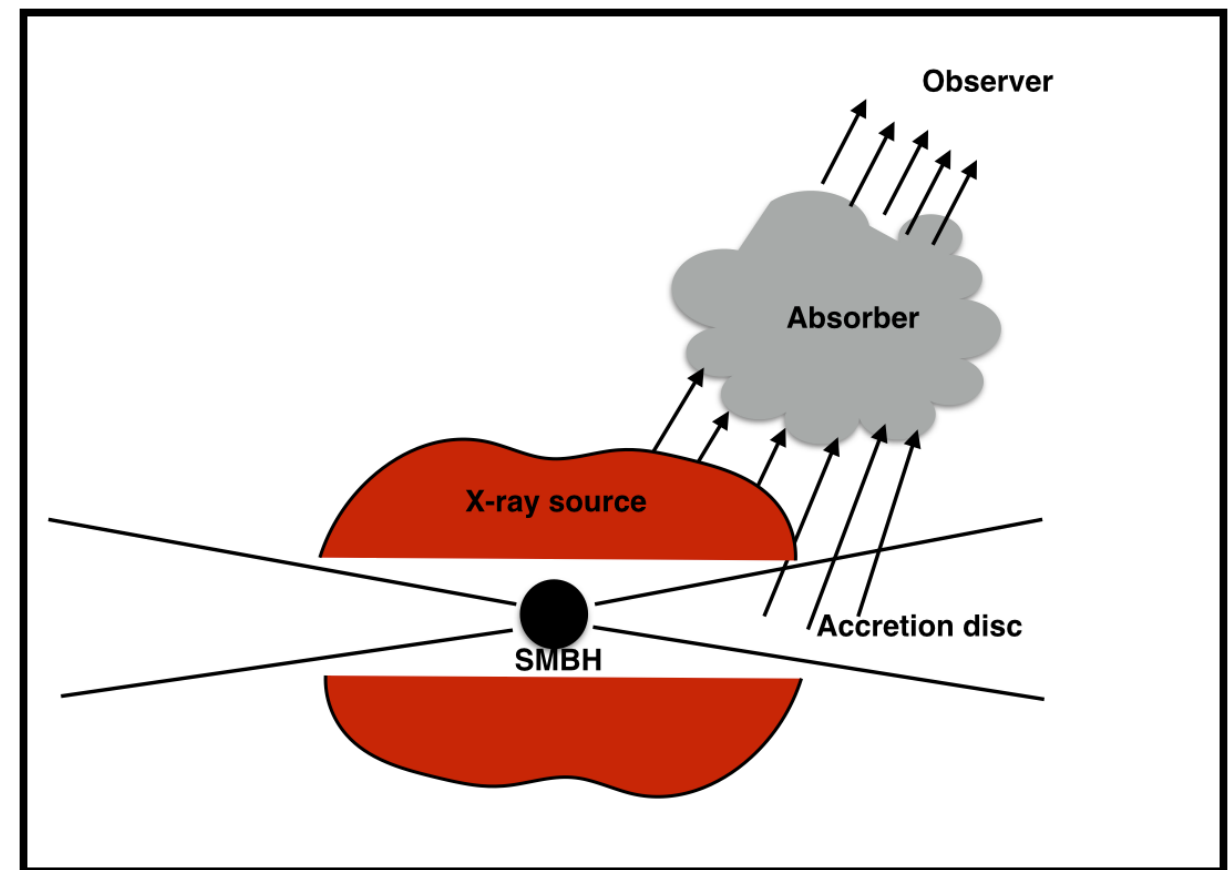


Collaborators  
Agata Różańska, Bożena Czerny, Krzysztof Hryniewicz

AGN Winds on the Georgia Coast , 25-29 June 2017

# Outline

- Absorption Measure Distribution (AMD) in AGNs: definition and observational motivation
- Photoionisation modelling of AMD
- Results from our modelling using TITAN (Dumont+ 2000) photoionisation code
- Summary



# Absorption measure distribution (AMD) in AGNs : from observations

Holczer+ 2007

- AMD requires  $\xi$  and  $N_H$

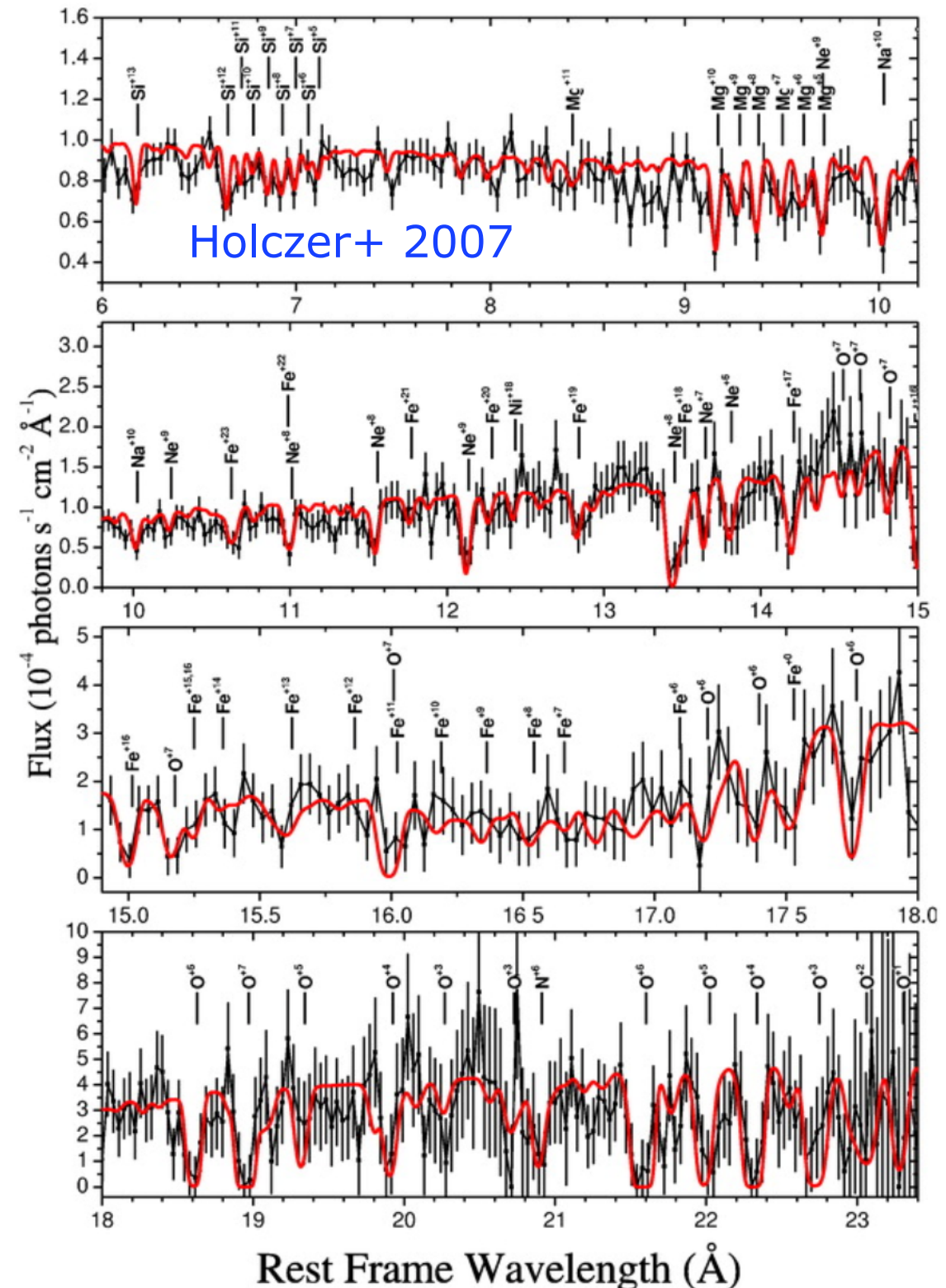
$$AMD = dN_H/d(\log \xi), \quad \xi = L/nR^2$$

$$N_H = \int AMD d(\log \xi).$$

- $N_{ion}$  is derived by fitting Gaussian profiles to the X-ray absorption lines in the observed spectra

$$N_{ion} = A_z \int \frac{dN_H}{d(\log \xi)} f_{ion}(\log \xi) d(\log \xi).$$

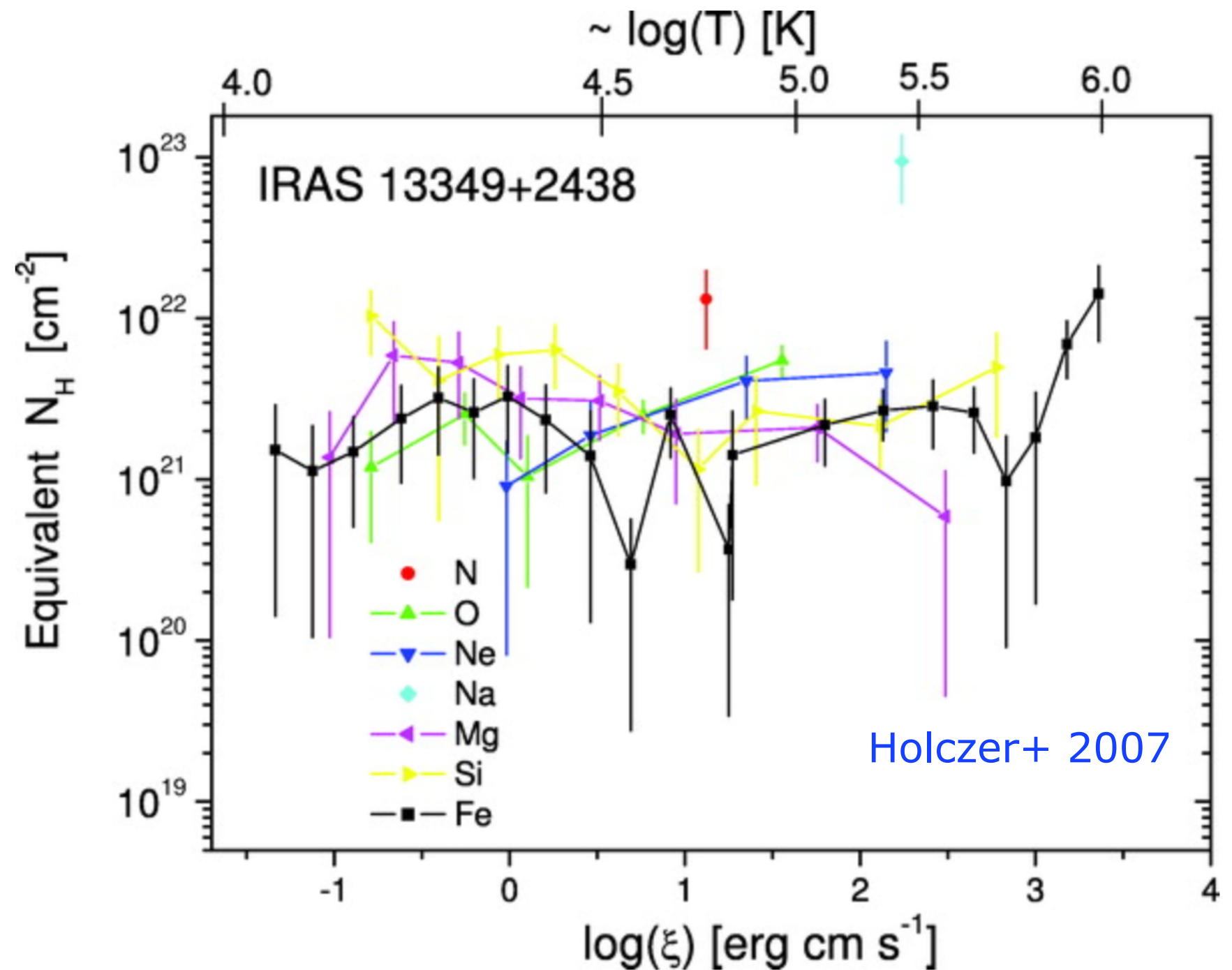
- $\xi$  and  $f_{ion}$  are computed from photoionisation models



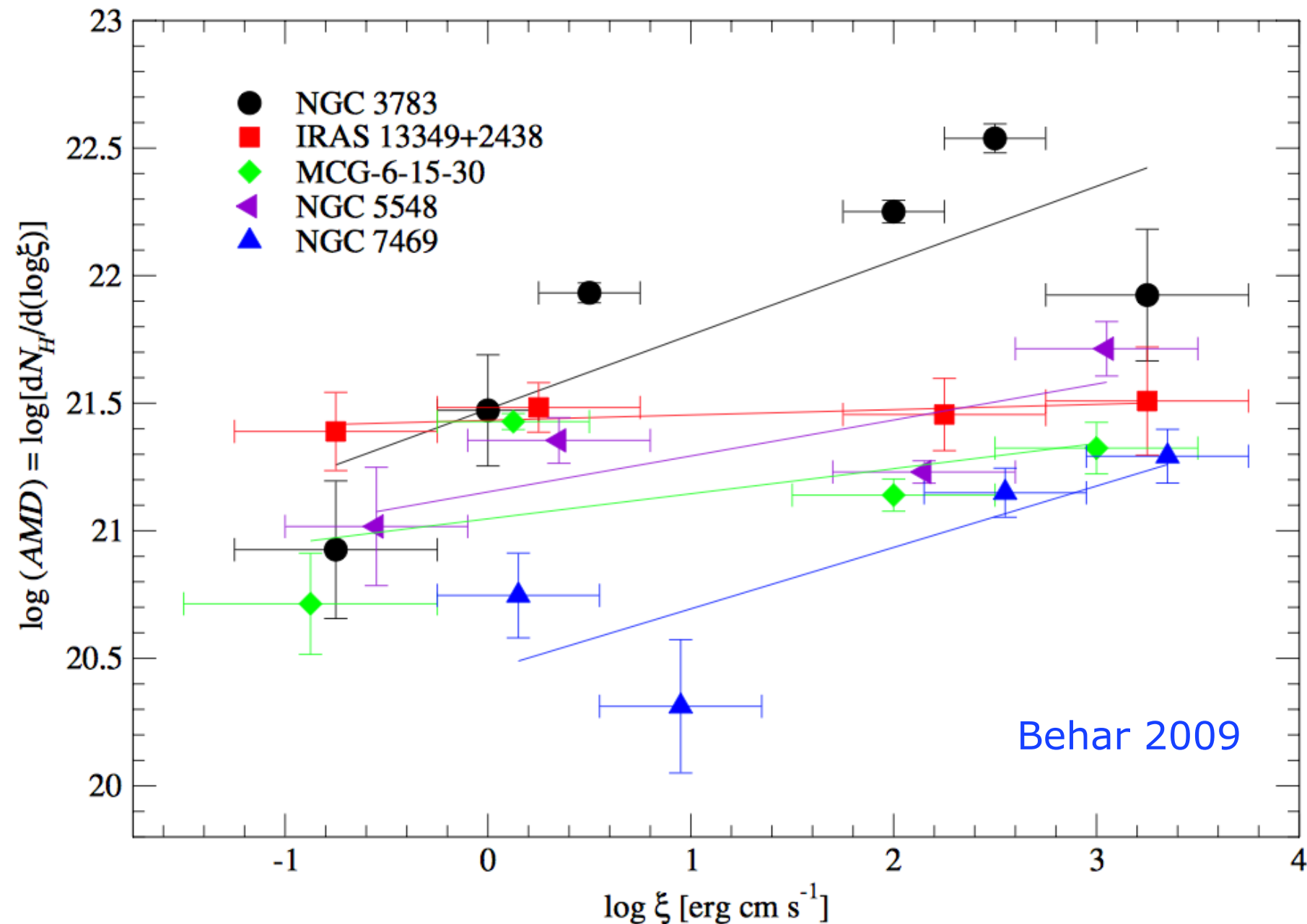
# Equivalent H- column densities

Importance of different ions, Fe in particular

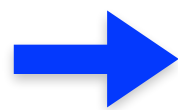
$$N_H \simeq \frac{N_{\text{ion}}}{f_{\text{ion}}(\xi_{\text{max}}) A_{Z_{\odot}}}$$



# Absorption measure distribution (AMD): Observation

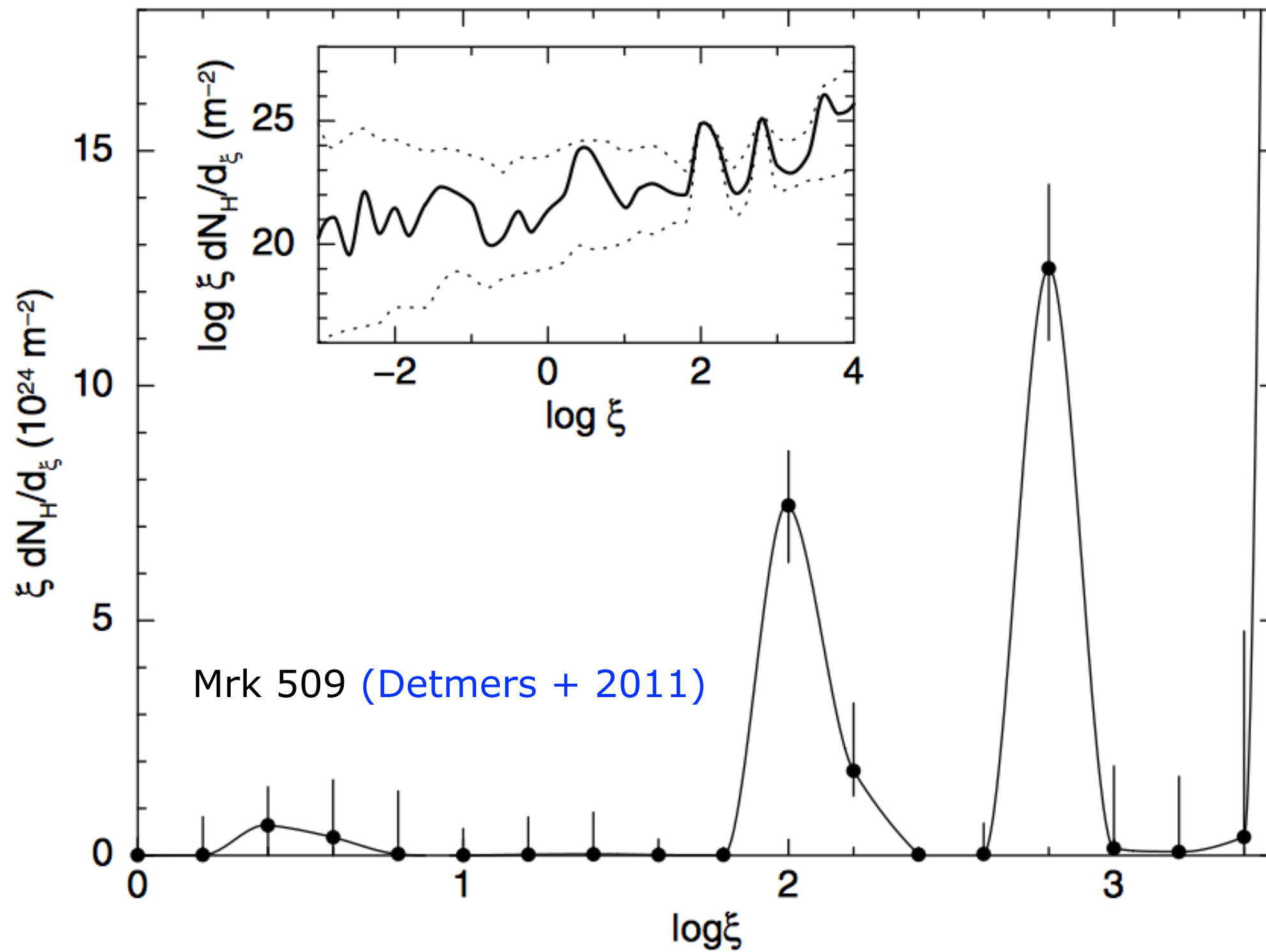


Discontinuity in  
the observed AMD



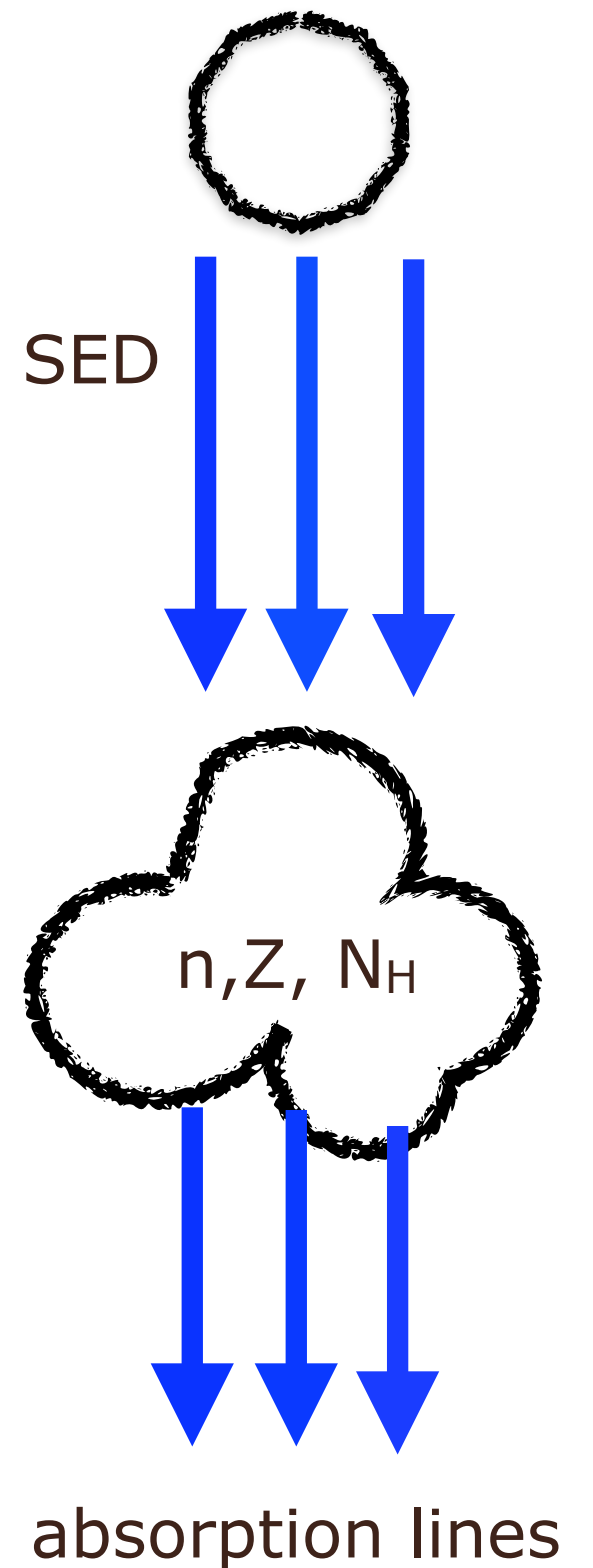
Observational evidence of Thermal  
instability (TI)? [Holczer + 2007](#), [Behar 2009](#)

# Absorption measure distribution (AMD): Observation



# Absorption measure distribution (AMD): Modelling

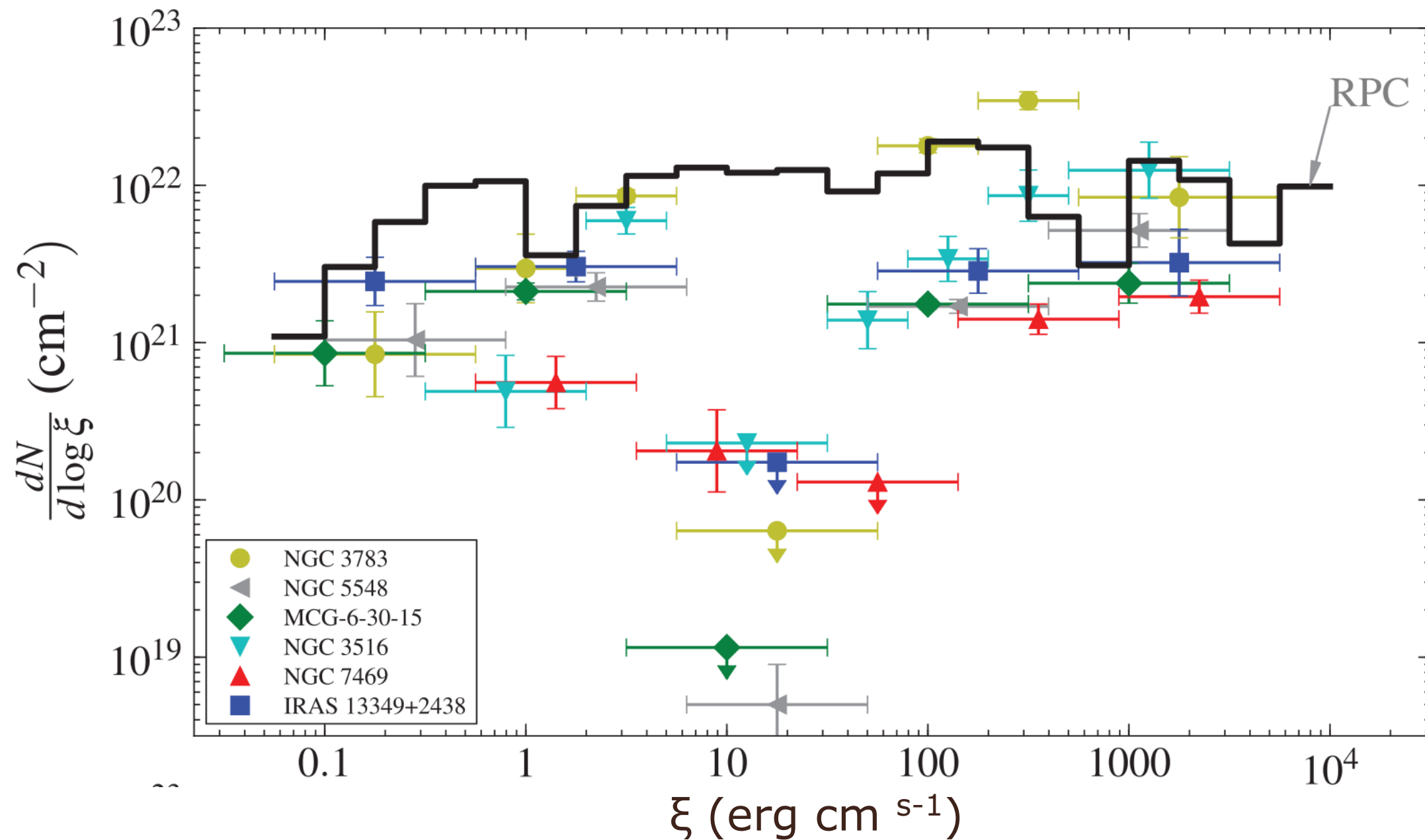
- Broad band SED
- Gas density  $n$
- Metallicity  $Z$
- Column Density  $N_H$
- Ionisation parameter,  $\xi = L/nR^2$
- Solving the radiative transfer, ionisation equilibrium and thermal balance
- Main Codes: CLOUDY (Ferland +2013), **TITAN** (Dumont+ 2000), XSTAR (Kallman & Bautista 2001),...





## AMD: models

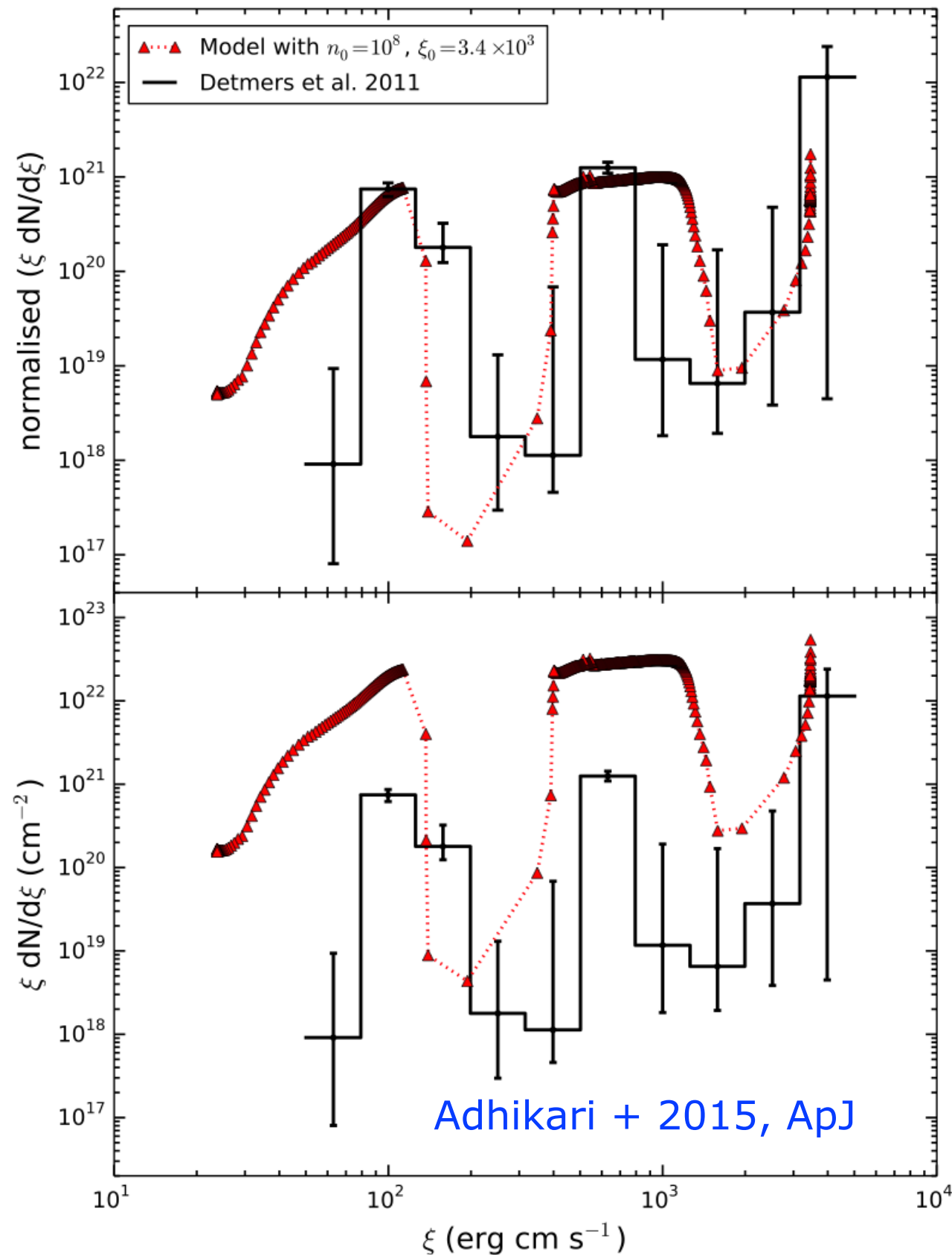
Radiation Pressure Confinement (RPC)  
model (Stern+ 2014) using CLOUDY



RPC model in CLOUDY did not reproduce TI



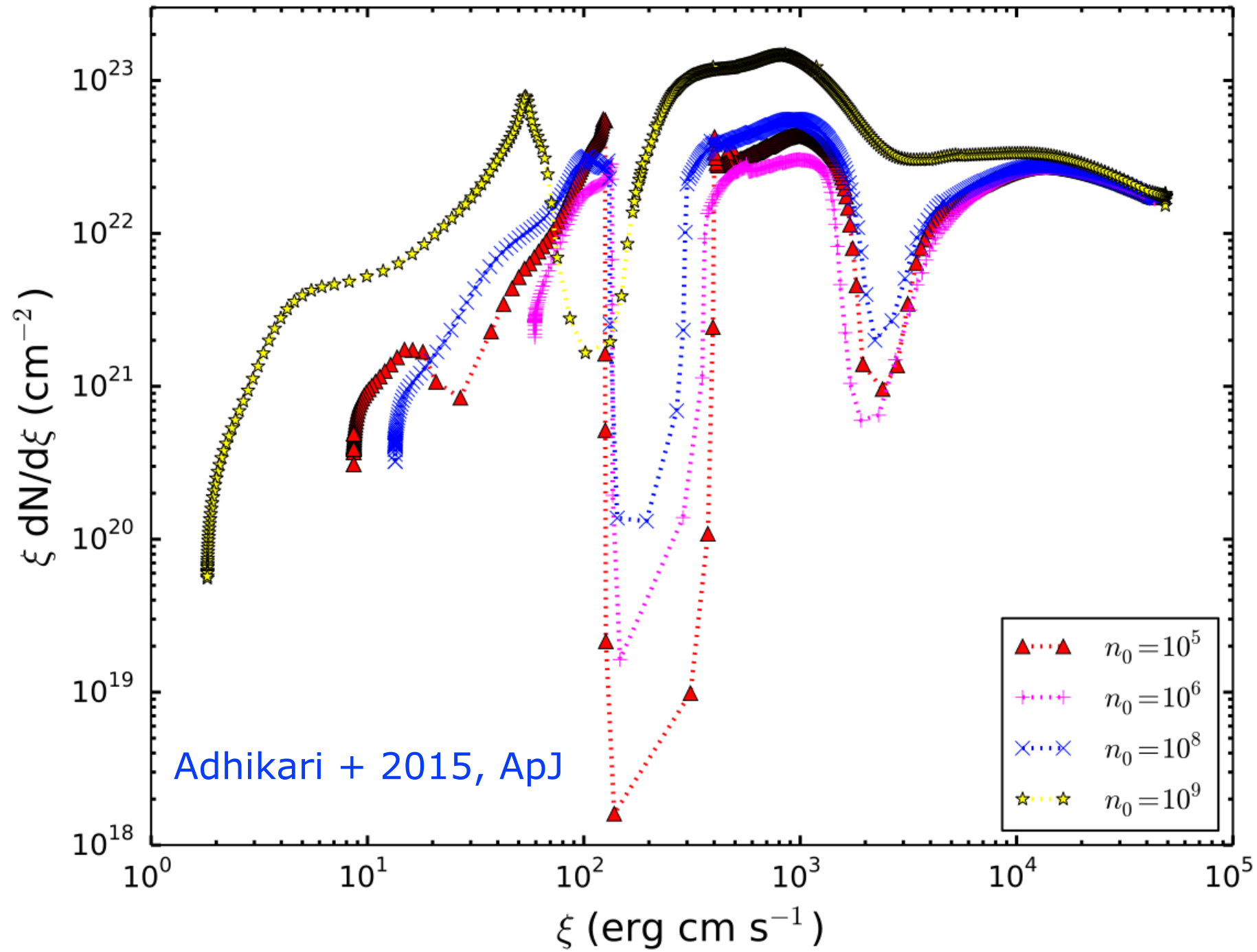
# AMD in Mrk 509: constant total pressure ( $P_{\text{gas}}+P_{\text{rad}}$ ) single model



TITAN code reproduces TI

problem with the normalisation!

## Density dependence of AMD



for Mrk 509 SED, the position of AMD dip depends on density

# RPC in Cloudy versus constant pressure in TITAN

## TITAN (Constant total pressure )

- more accurate Accelerated Lambda Iteration (ALI) method

$$\mu \frac{dl_\nu}{d\tau_\nu} = l_\nu - \frac{j_\nu}{\kappa_\nu + \sigma_\nu} = l_\nu - S_\nu$$

- radiation pressure is computed from radiation field and goes into the gas structure directly

## CLOUDY (RPC)

- Escape probability method of radiative transfer

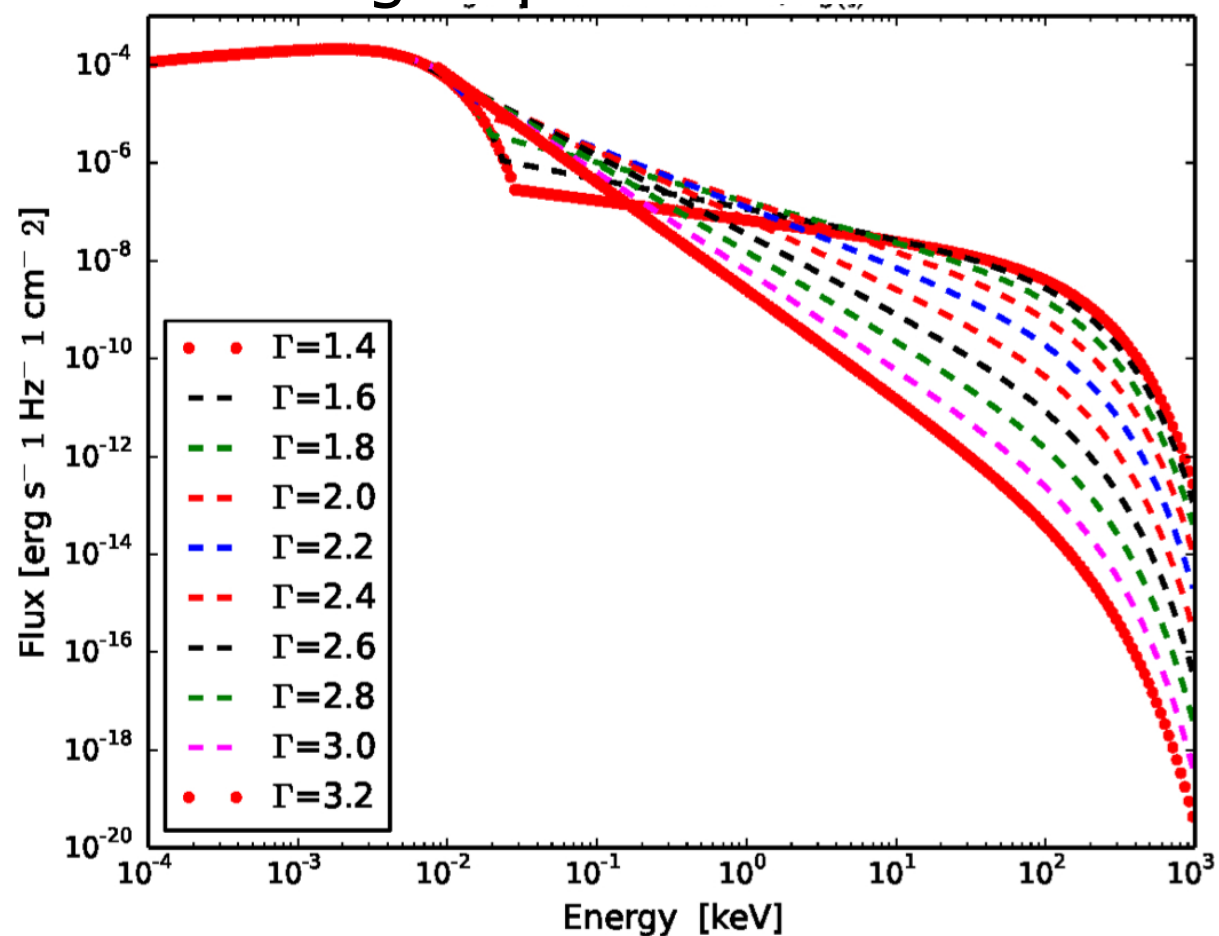
$$dP_{gas}(\tau) = P_{rad}e^{-\tau}d\tau$$

- pressure induced by the trapped emitted radiation is not considered

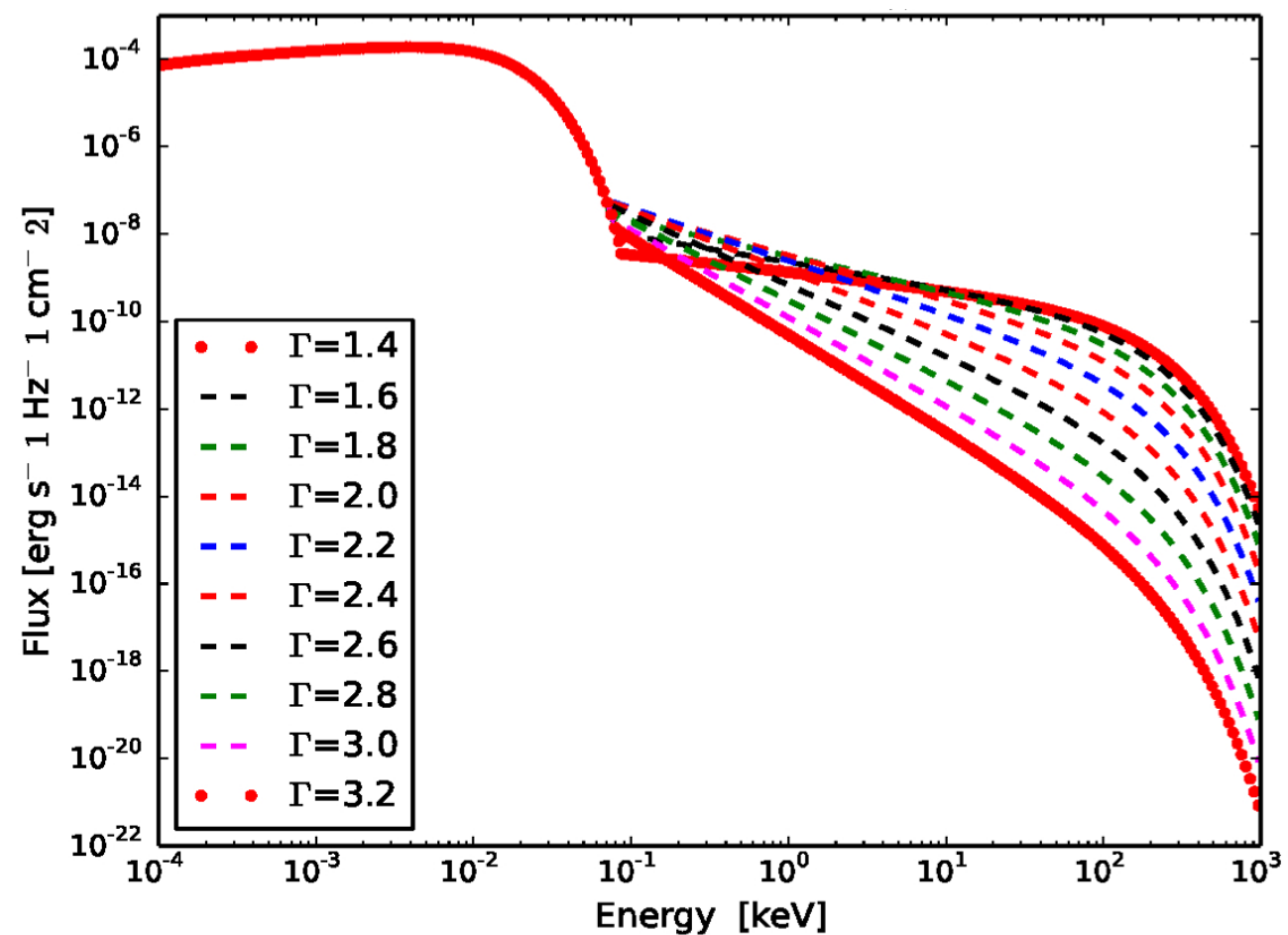
Escape probability method versus ALI method ([Dumont+ 2003](#))

# Systematic study of AMD using TITAN

high-spin-low-mdotr

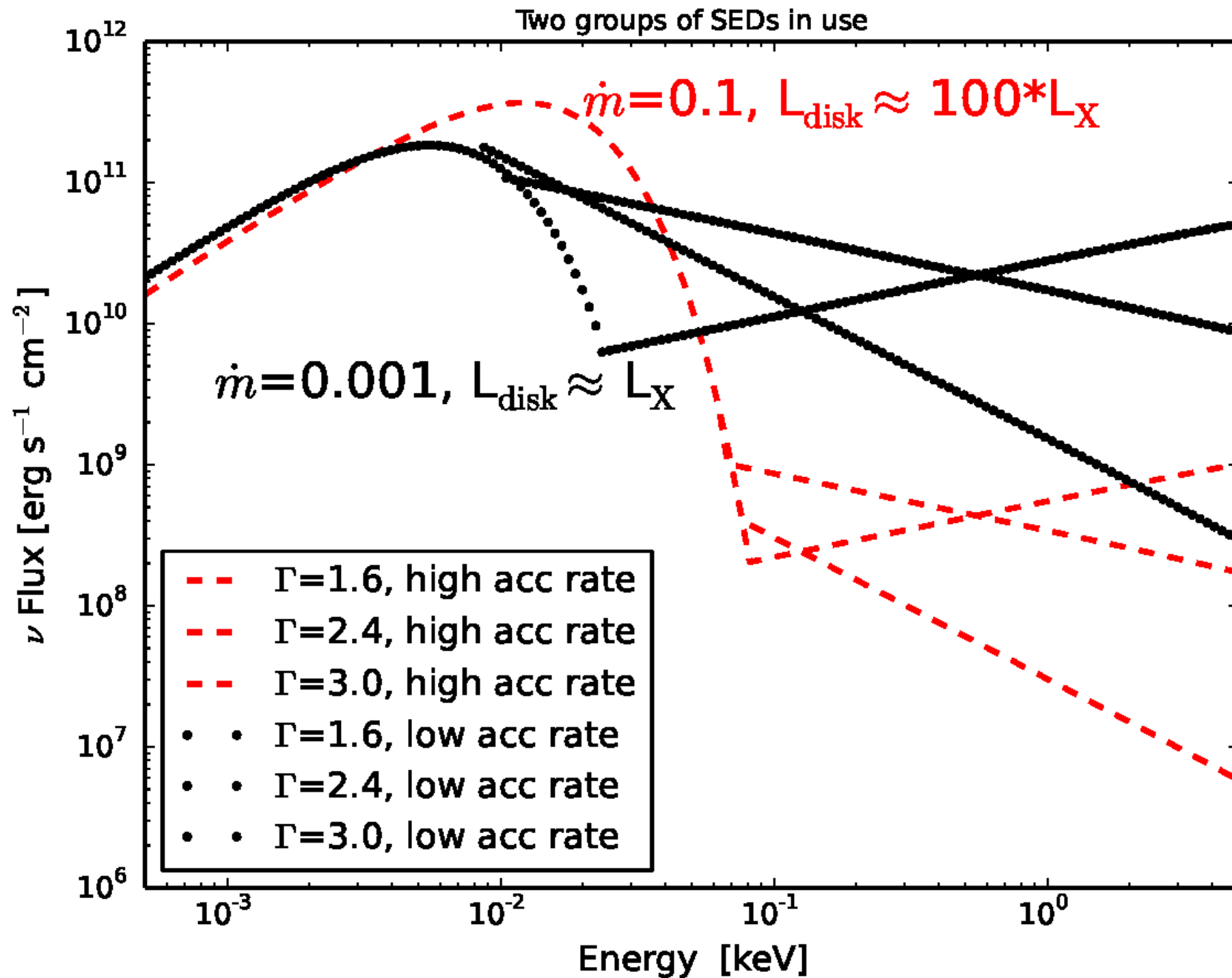


low-spin-high-mdotr



Adhikari+ 2017, in preparation

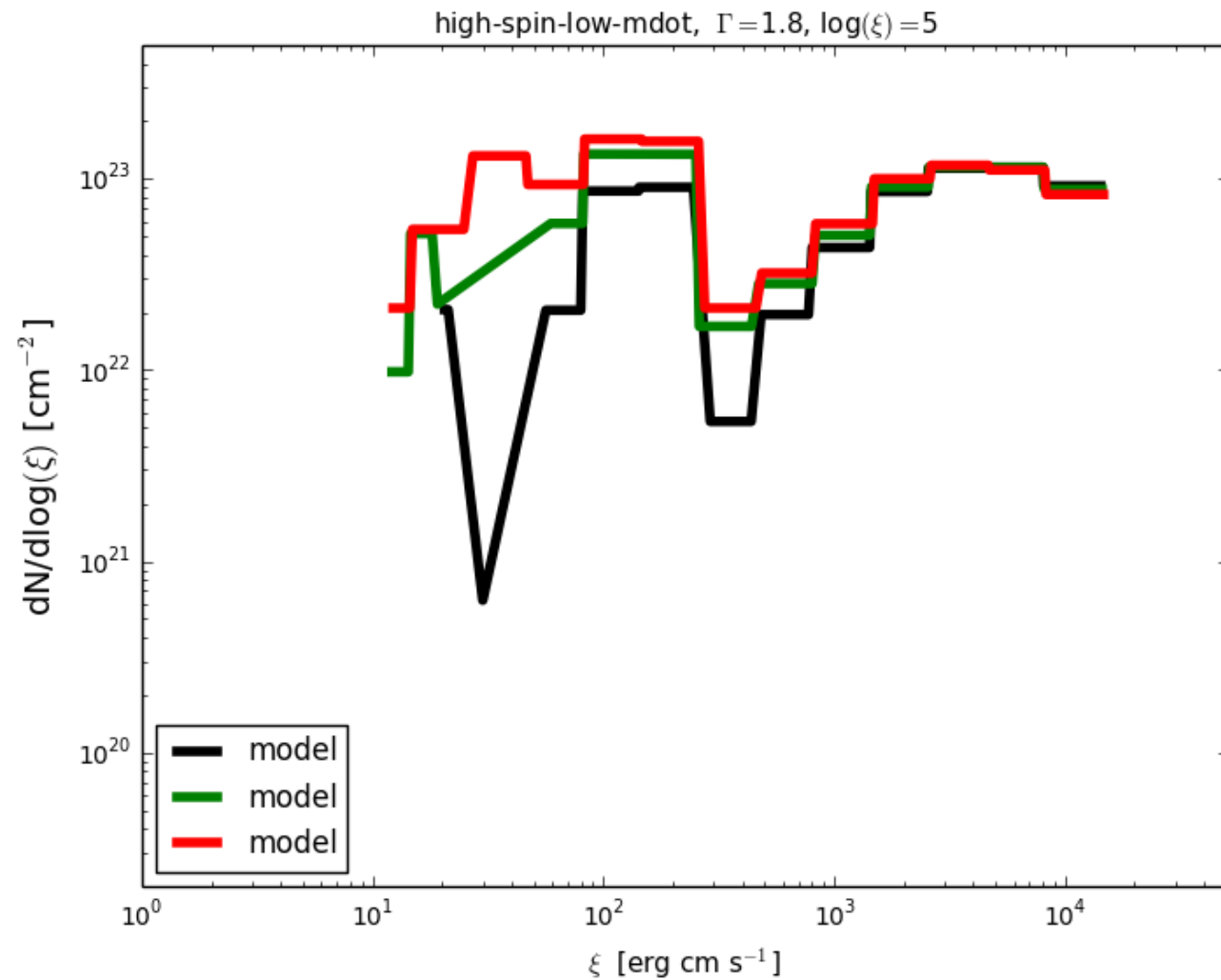
# Systematic study of AMD using TITAN



# Systematic study of AMD using TITAN: normalisation and position of dip in AMD

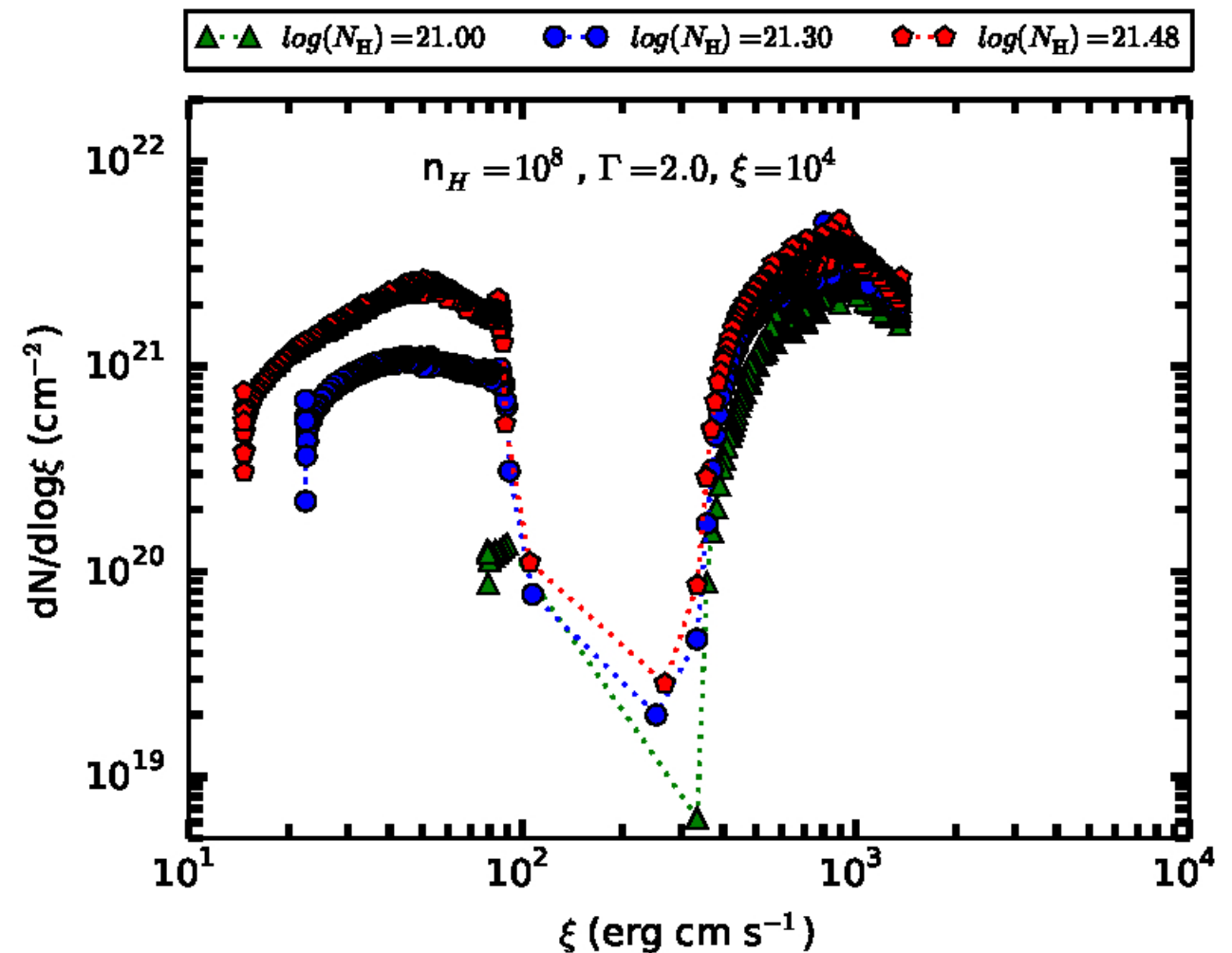
$$N_H \geq 10^{23} \text{ cm}^{-2}$$

SED - with strong X-ray illumination



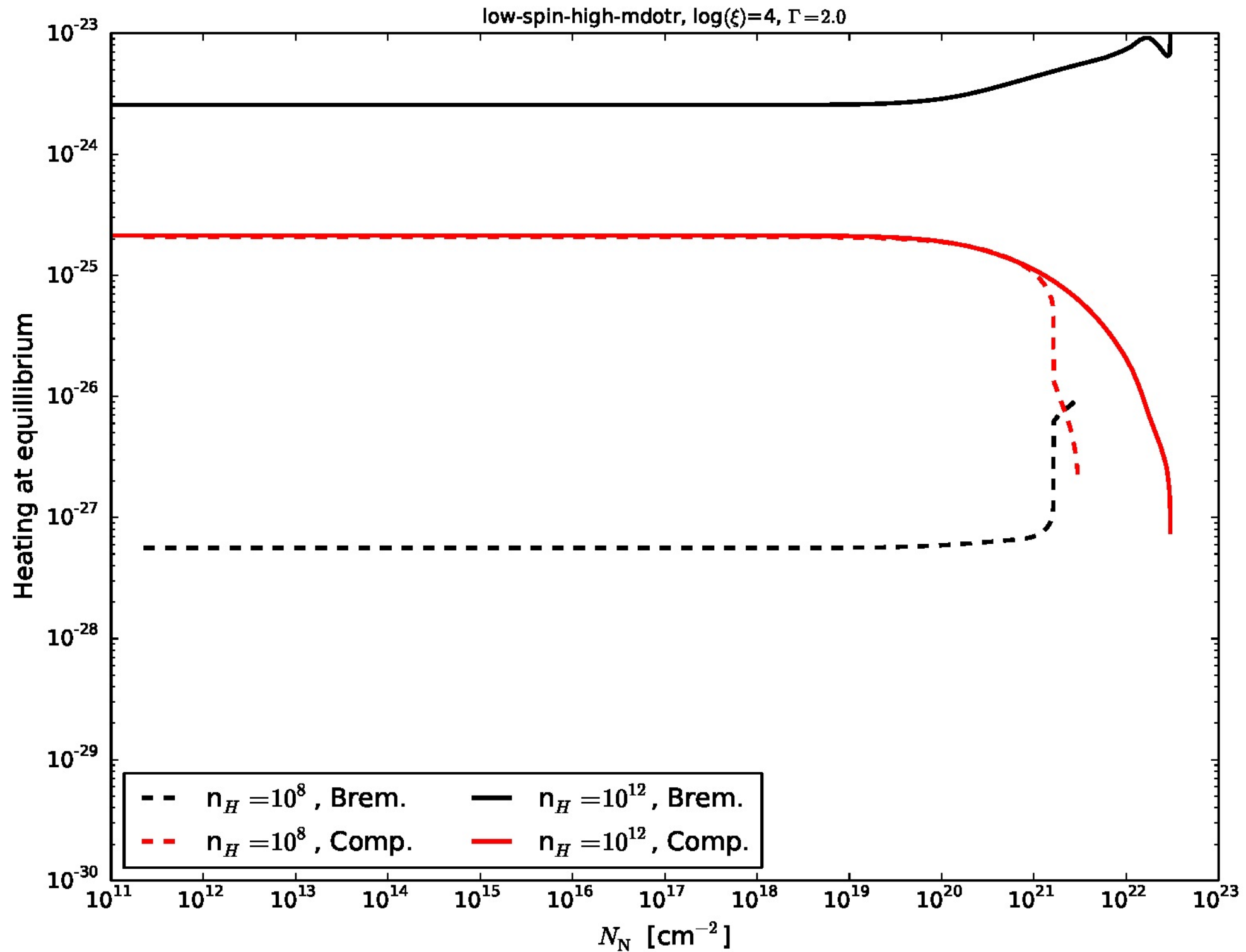
$$N_H \sim 10^{21} - 10^{22} \text{ cm}^{-2}$$

SED- with strong opt/UV component



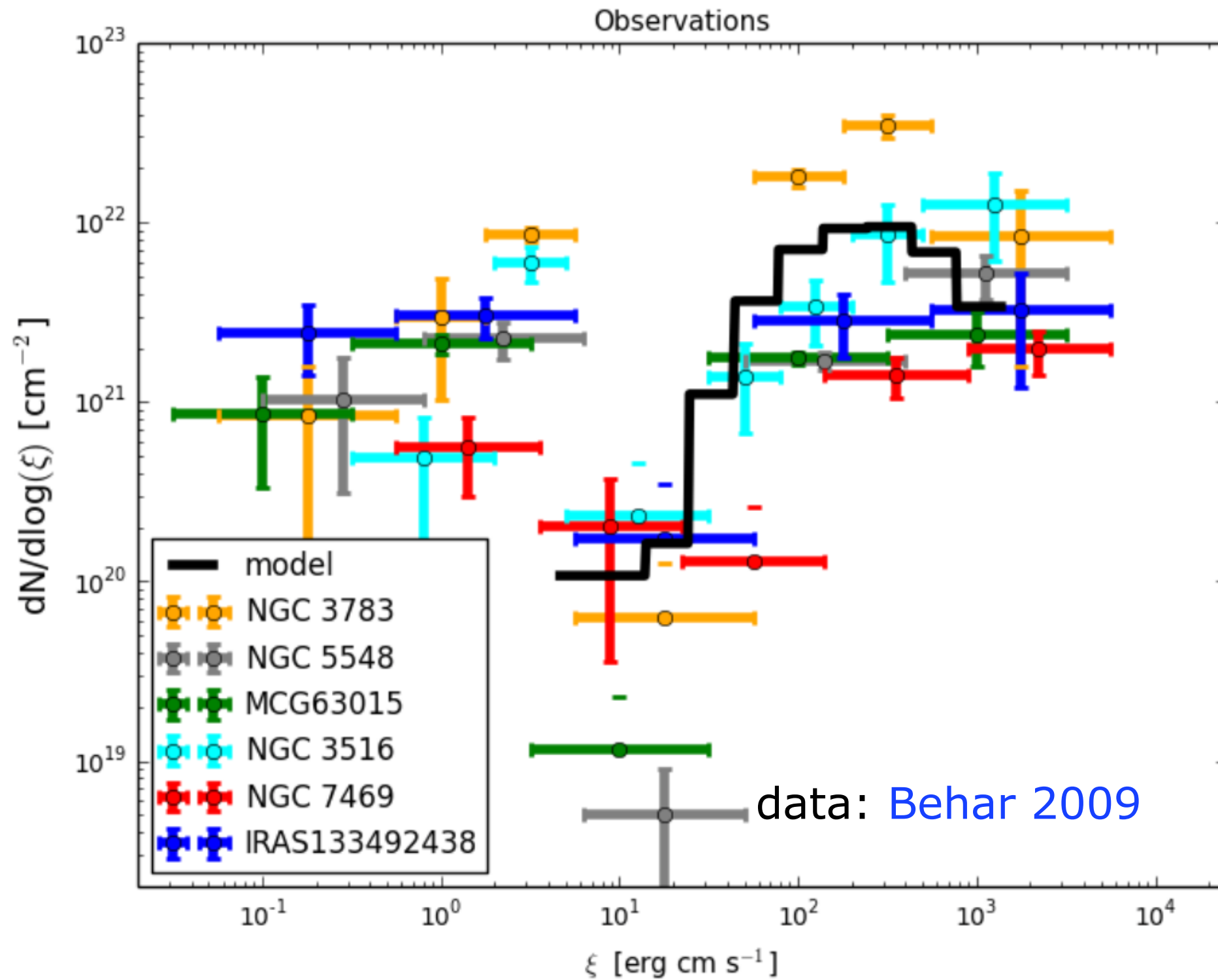
Adhikari+ 2017, in preparation

normalisation is higher for SED with strong X-ray illumination



In case of SED with strong optical/UV component and for high density, free free heating dominates over the Compton heating





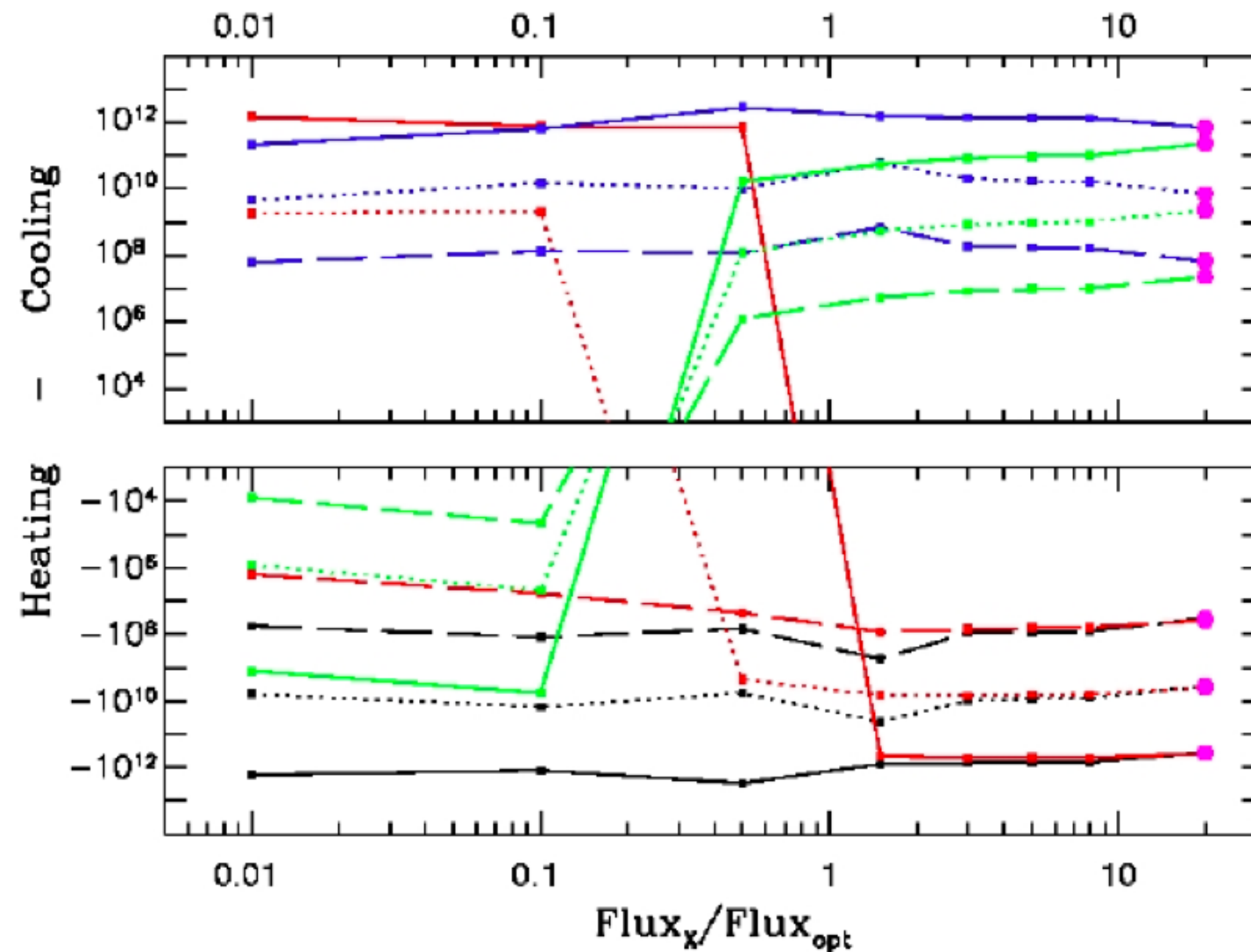
TITAN model: SED with with strong optical/  
UV component,  $\log N_H = 22.48$ ,  $\log n_H = 12$

## Summary

- Constant total pressure single component WA model explains the observed AMD in Mrk 509.
- Computations of AMDs with the constant pressure assumption for different SED components shows that the normalisation is higher for SED with strong X-ray illumination and weak optical/UV component.
- For the given SED, the position of AMD dip depends on the density of the absorber.

Back up slides...

Róžańska +08, **Processes**



Net bound-free (Ion. – Rec.)

Net free-free (H – C)

Net Compton (H – C)

Net bound-bound (H – C) LINES

Solid line –  $n = 10^{10} \text{ cm}^{-3}$

Dotted line –  $n = 10^8 \text{ cm}^{-3}$

Dashed line –  $n = 10^6 \text{ cm}^{-3}$